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#### Aims and Motivation for the Course

#### We aim to:

- Develop a theory which can characterize the behavior of real-world Random Signals and Processes;
- Use standard **Probability Theory** for this.

# Random signal theory is important for

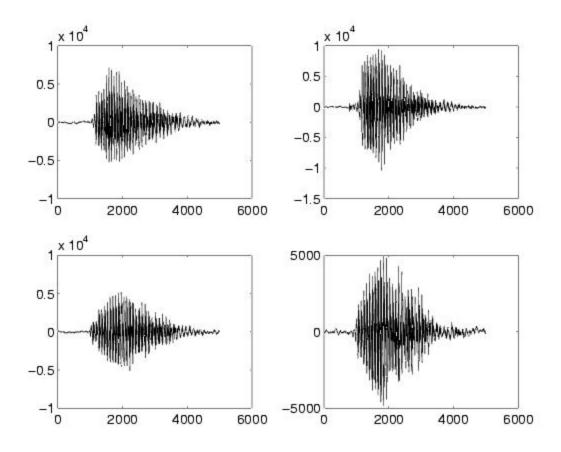
- Analysis of signals;
- Inference of underlying system parameters from noisy observed data;
- Design of optimal systems (digital and analogue signal recovery, signal classification, estimation ...);
- Predicting system performance (error-rates, signal-to-noise ratios, ...).

# Example:

# Speech signals

Use probability theory to characterize that some sequences of vowels and consonants are more likely than others, some waveforms more likely than others for a given vowel or consonant. Please see [link].

Use this to achieve: speech recognition, speech coding, speech enhancement, ...



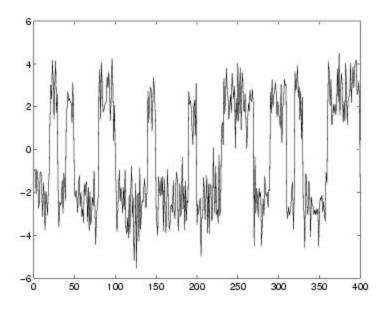
Four utterances of the vowel sound 'Aah'.

# **Example:**

# **Digital communications**

Characterize the properties of the digital data source (mobile phone, digital television transmitter, ...), characterize the noise/distortions present in the transmission channel. Please see [link].

Use this to achieve: accurate regeneration of the digital signal at the receiver, analysis of the channel characteristics ...



Digital data stream from a noisy communications Channel.

Probability theory is used to give a mathematical description of the behavior of real-world systems which involve elements of **randomness**. Such a system might be as simple as a coin-flipping experiment, in which we are interested in whether 'Heads' or 'Tails' is the outcome, or it might be more complex, as in the study of random errors in a coded digital data stream (e.g. a CD recording or a digital mobile phone).

The basics of probability theory should be familiar from the IB Probability and Statistics course. Here we summarize the main results from that course and develop them into a framework that can encompass random signals and processes.

## **Probability Distributions**

The distribution  $P_X$  of a random variable X is simply a probability measure which assigns probabilities to events on the real line. The distribution  $P_X$  answers questions of the form:

What is the probability that X lies in some subset F of the real line?

In practice we summarize  $P_X$  by its **Probability Mass Function - pmf** (for discrete variables only), **Probability Density Function - pdf** (mainly for continuous variables), or **Cumulative Distribution Function - cdf** (for either discrete or continuous variables).

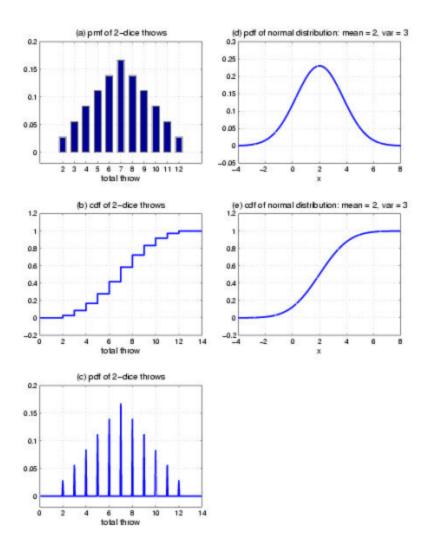
# **Probability Mass Function (pmf)**

Suppose the discrete random variable X can take a set of M real values  $\{x_1, ..., x_M\}$ , then the **pmf** is defined as:

### **Equation:**

$$egin{array}{lll} p_X(x_i) &=& \Pr[X=x_i] \ &=& P_X(\{x_i\}) \end{array}$$

where  $\sum_{i=1}^{M} p_X(x_i) = 1$ . e.g. For a normal 6-sided die, M = 6 and  $p_X(x_i) = \frac{1}{6}$ . For a pair of dice being thrown, M = 11 and the pmf is as shown in (a) of [link].



Examples of pmfs, cdfs and pdfs: (a) to (c) for a discrete process, the sum of two dice; (d) and (e) for a continuous process with a normal or Gaussian distribution, whose mean = 2 and variance = 3.

# **Cumulative Distribution Function (cdf)**

The  $\mathbf{cdf}$  can describe discrete, continuous or mixed distributions of X and is defined as:

$$F_X(x) = \Pr[X \le x]$$
  
=  $P_X((-\infty, x])$ 

For discrete *X*:

### **Equation:**

$$F_X(x) = \sum_i \{p_X(x_i)|\, x_i \leq x\}$$

giving step-like cdfs as in the example of (b) of [link].

Properties follow directly from the Axioms of Probability:

- 1.  $0 \le F_X(x) \le 1$
- 2.  $F_X(-\infty) = 0, F_X(\infty) = 1$
- 3.  $F_X(x)$  is non-decreasing as x increases
- 4.  $\Pr[x_1 < X \le x_2] = F_X(x_2) F_X(x_1)$
- 5.  $\Pr[X > x] = 1 F_X(x)$

where there is no ambiguity we will often drop the subscript X and refer to the cdf as F(x).

# **Probability Density Function (pdf)**

The **pdf** of *X* is defined as the derivative of the cdf:

# **Equation:**

$$f_X(x) = rac{\mathrm{d}}{\mathrm{d}\ x} F_X(x)$$

The pdf can also be interpreted in derivative form as  $\delta(x) \to 0$ :

$$egin{array}{lll} f_X(x)\delta(x) &=& \Pr[x < X \leq x + \delta(x)] \ &=& F_X(x + \delta(x)) - F_X(x) \end{array}$$

For a discrete random variable with pmf given by  $p_X(x_i)$ :

# **Equation:**

$$f_X(x) = \sum_{i=1}^M p_X(x_i) \delta(x-x_i)$$

An example of the pdf of the 2-dice discrete random process is shown in (c) of [link]. (Strictly the delta functions should extend vertically to infinity, but we show them only reaching the values of their areas,  $p_X(x_i)$ .)

The pdf and cdf of a continuous distribution (in this case the **normal** or **Gaussian** distribution) are shown in (d) and (e) of [link].

**Note:** The cdf is the integral of the pdf and should always go from zero to unity for a valid probability distribution.

Properties of pdfs:

- 1.  $f_X(x) \geq 0$ 2.  $\int_{-\infty}^{\infty} f_X(x) \ \mathrm{d} \ x = 1$
- 3.  $F_X(x) = \int_{-\infty}^x f_X(\alpha) d\alpha$
- 4.  $\Pr[x_1 < X \leq x_2] = \int_{x_1}^{x_2} f_X(\alpha) d\alpha$

As for the cdf, we will often drop the subscript X and refer simply to f(x)when no confusion can arise.

# Conditional Probabilities and Bayes' Rule

If *A* and *B* are two separate but possibly dependent random events, then:

- 1. Probability of A and B occurring together = Pr[A, B]
- 2. The conditional probability of A, given that B occurs =  $Pr[A \mid B]$
- 3. The conditional probability of B, given that A occurs =  $Pr[B \mid A]$

From elementary rules of probability (Venn diagrams):

### **Equation:**

$$Pr[A, B] = Pr[A \mid B] Pr[B]$$
$$= Pr[B \mid A] Pr[A]$$

Dividing the right-hand pair of expressions by  $\Pr[B]$  gives Bayes' rule: **Equation:** 

$$\Pr[A \mid B] = rac{\Pr[B \mid A] \Pr[A]}{\Pr[B]}$$

In problems of probabilistic inference, we are often trying to estimate the most probable underlying model for a random process, based on some observed data or evidence. If A represents a given set of model parameters, and B represents the set of observed data values, then the terms in  $[\underline{link}]$  are given the following terminology:

- Pr[A] is the **prior** probability of the model A (in the absence of any evidence);
- Pr[B] is the probability of the **evidence** B;
- $Pr[B \mid A]$  is the **likelihood** that the evidence B was produced, given that the model was A;
- $Pr[A \mid B]$  is the **posterior** probability of the model being A, given that the evidence is B.

Quite often, we try to find the model A which maximizes the posterior  $\Pr[A \mid B]$ . This is known as **maximum a posteriori** or **MAP** model

selection.

The following example illustrates the concepts of Bayesian model selection.

# Example:

### **Loaded Dice**

Problem:

Given a tub containing 100 six-sided dice, in which one die is known to be loaded towards the six to a specified extent, derive an expression for the probability that, after a given set of throws, an arbitrarily chosen die is the loaded one? Assume the other 99 dice are all fair (not loaded in any way). The loaded die is known to have the following pmf:

$$p_L(1) = 0.05$$
  $\{p_L(2), \ldots, p_L(5)\} = 0.15$   $p_L(6) = 0.35$ 

Here derive a good strategy for finding the loaded die from the tub. Solution:

The pmfs of the fair dice may be assumed to be:

$$orall i, i = \{1, \ldots, 6\}: \left(p_F(i) = rac{1}{6}
ight)$$

Let each die have one of two states, S = L if it is loaded and S = F if it is fair. These are our two possible **models** for the random process and they have underlying pmfs given by  $\{p_L(1), \ldots, p_L(6)\}$  and  $\{p_F(1), \ldots, p_F(6)\}$  respectively.

After N throws of the chosen die, let the sequence of throws be  $\Theta_N = \{\theta_1, \ldots, \theta_N\}$ , where each  $\theta_i \in \{1, \ldots, 6\}$ . This is our **evidence**. We shall now calculate the probability that this die is the loaded one. We therefore wish to find the **posterior**  $\Pr[S = L \mid \Theta_N]$ .

We cannot evaluate this directly, but we can evaluate the **likelihoods**,  $\Pr[\Theta_N \mid S = L]$  and  $\Pr[\Theta_N \mid S = F]$ , since we know the expected pmfs

in each case. We also know the **prior** probabilities  $\Pr[S=L]$  and  $\Pr[S=F]$  before we have carried out any throws, and these are  $\{0.01,0.99\}$  since only one die in the tub of 100 is loaded. Hence we can use Bayes' rule:

### **Equation:**

$$\Pr[S = L \mid \Theta_N] = rac{\Pr[\Theta_N \mid S = L] \Pr[S = L]}{\Pr[\Theta_N]}$$

The denominator term  $\Pr[\Theta_N]$  is there to ensure that  $\Pr[S=L\mid\Theta_N]$  and  $\Pr[S=F\mid\Theta_N]$  sum to unity (as they must). It can most easily be calculated from:

### **Equation:**

$$egin{array}{lll} \Pr[\Theta_N] &=& \Pr[\Theta_N,S=L] + \Pr[\Theta_N,S=F] \ &=& \Pr[\Theta_N \mid S=L] \Pr[S=L] + \Pr[\Theta_N \mid S=F] \Pr[S=F] \end{array}$$

so that

### **Equation:**

$$egin{array}{lll} \Pr[S=L \mid oldsymbol{arTheta}_N] &=& rac{\Pr[oldsymbol{arTheta}_N \mid S=L] \Pr[S=L]}{\Pr[oldsymbol{arTheta}_N \mid S=L] \Pr[S=L] + \Pr[oldsymbol{arTheta}_N \mid S=F] \Pr[S=F]} \ &=& rac{1}{1+R_N} \end{array}$$

where

# **Equation:**

$$R_N = rac{\Pr[\Theta_N \mid S=F] \Pr[S=F]}{\Pr[\Theta_N \mid S=L] \Pr[S=L]}$$

To calculate the likelihoods,  $\Pr[\Theta_N \mid S = L]$  and  $\Pr[\Theta_N \mid S = F]$ , we simply take the product of the probabilities of each throw occurring in the sequence of throws  $\Theta_N$ , given each of the two modules respectively (since each new throw is independent of all previous throws, given the model). So, after N throws, these likelihoods will be given by:

$$\Pr[\Theta_N \mid S = L] = \prod_{i=1}^N p_L( heta_i)$$

and

### **Equation:**

$$\Pr[\Theta_N \mid S = F] = \prod_{i=1}^N p_F( heta_i)$$

We can now substitute these probabilities into the above expression for  $R_N$  and include  $\Pr[S=L]=0.01$  and  $\Pr[S=F]=0.99$  to get the desired a **posteriori** probability  $\Pr[S=L\mid\Theta_N]$  after N throws using [link]. We may calculate this iteratively by noting that

### **Equation:**

$$\Pr[\Theta_N \mid S = L] = \Pr[\Theta_{N-1} \mid S = L] p_L(\theta_n)$$

and

### **Equation:**

$$\Pr[\Theta_N \mid S = F] = \Pr[\Theta_{N-1} \mid S = F] p_F(\theta_n)$$

so that

# **Equation:**

$$R_N = R_{N-1} rac{p_F( heta_n)}{ ext{mfrac}}$$

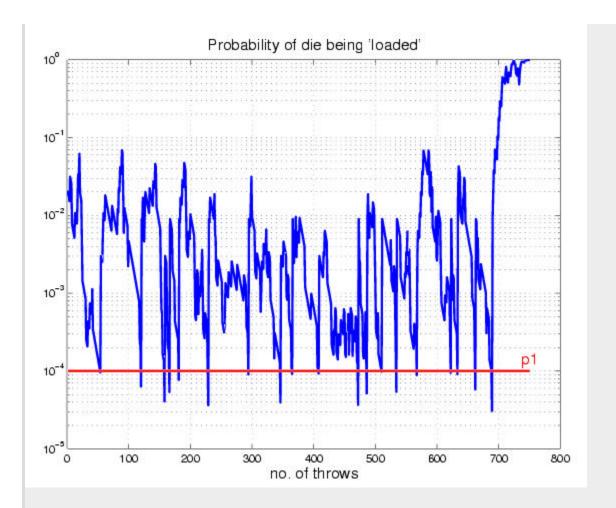
where  $R_0 = \frac{\Pr[S=F]}{\Pr[S=L]} = 99$ . If we calculate this after every throw of the current die being tested (i.e. as N increases), then we can either move on to test the next die from the tub if  $\Pr[S=L\mid\Theta_N]$  becomes sufficiently small (say  $<(10^{-4})$ ) or accept the current die as the loaded one when  $\Pr[S=L\mid\Theta_N]$  becomes large enough (say >(0.995)). (These thresholds correspond approximately to  $R_N>10^4$  and  $R_N<5\times10^{-3}$  respectively.)

The choice of these thresholds for  $\Pr[S=L\mid\Theta_N]$  is a function of the desired tradeoff between speed of searching versus the probability of failure to find the loaded die, either by moving on to the next die even when the current one is loaded, or by selecting a fair die as the loaded one. The lower threshold,  $p_1=10^{-4}$ , is the more critical, because it affects how long we spend before discarding each fair die. The probability of correctly detecting all the fair dice before the loaded die is reached is  $(1-p_1)^n \simeq 1-np_1$ , where  $n \simeq 50$  is the expected number of fair dice tested before the loaded one is found. So the failure probability due to incorrectly assuming the loaded die to be fair is approximately  $np_1 \simeq 0.005$ .

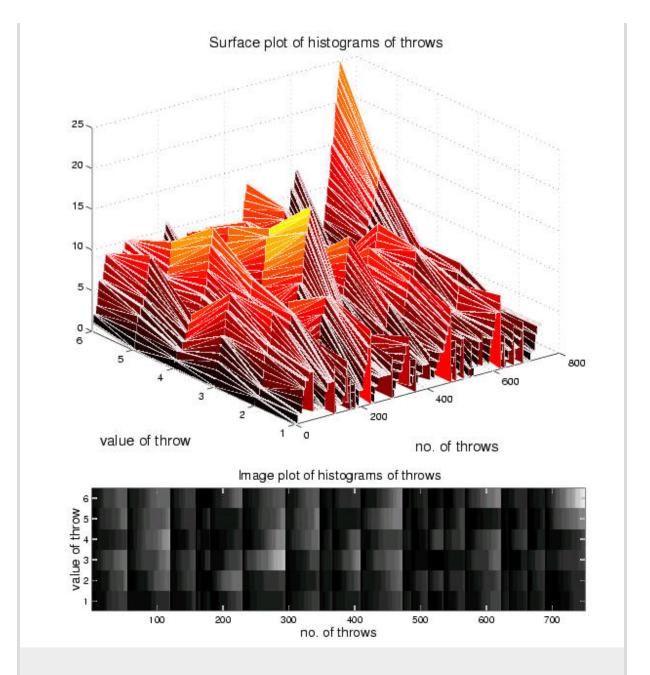
The upper threshold,  $p_2 = 0.995$ , is much less critical on search speed, since the **loaded** result only occurs once, so it is a good idea to set it very close to unity. The failure probability caused by selecting a fair die to be the loaded one is just  $1 - p_2 = 0.005$ . Hence the overall failure probability = 0.005 + 0.005 = 0.01

**Note:** In problems with significant amounts of evidence (e.g. large N), the evidence probability and the likelihoods can both get very very small, sufficient to cause floating-point underflow on many computers if equations such as  $[\underline{link}]$  and  $[\underline{link}]$  are computed directly. However the ratio of likelihood to evidence probability still remains a reasonable size and is an important quantity which must be calculated correctly.

One solution to this problem is to compute only the ratio of likelihoods, as in [link]. A more generally useful solution is to compute log(likelihoods) instead. The product operations in the expressions for the likelihoods then become sums of logarithms. Even the calculation of likelihood ratios such as  $R_N$  and comparison with appropriate thresholds can be done in the log domain. After this, it is OK to return to the linear domain if necessary since  $R_N$  should be a reasonable value as it is the **ratio** of very small quantities.



Probabilities of the current die being the loaded one as the throws progress (20th die is the loaded one). A new die is selected whenever the probability falls below  $p_1$ .



Histograms of the dice throws as the throws progress. Histograms are reset when each new die is selected.

# Joint and Conditional cdfs and pdfs

### **Cumulative distribution functions**

We define the **joint** cdf to be

### **Equation:**

$$F(x,y) = \Pr[(X \le x) \land (Y \le y)]$$

and conditional cdf to be

### **Equation:**

$$F(x|y) = \Pr[X \le x \mid Y \le y]$$

Hence we get the following rules:

• Conditional probability (cdf): Equation:

$$egin{array}{lcl} F(x|y) &=& \Pr[X \leq x \mid Y \leq y] \ &=& rac{F(x,y)}{F_Y(y)} \end{array}$$

• Bayes Rule (cdf): Equation:

$$F(x|y) = \frac{F(y|x)F(x)}{F(y)}$$

• Total probability (cdf): Equation:

$$F(x,\infty) = F(x)$$

which follows because the event  $Y \leq \infty$  itself forms a partition of the sample space.

Conditional cdf's have similar properties to standard cdf's, i.e.

$$F_{X|Y}(-\infty|y)=0$$

$$F_{X|Y}(\infty|y)=1$$

# **Probability density functions**

We define joint and conditional pdfs in terms of corresponding cdfs. The **joint** pad is defined to be

### **Equation:**

$$f(x,y) = rac{\partial^2 F(x,y)}{\partial x \partial y}$$

and the **conditional** pdf is defined to be

# **Equation:**

$$f(x|y) = rac{\partial rac{\mathrm{d} F(x|Y=y)}{\mathrm{d}}}{\partial x}$$

where

$$F'(x|Y=y) = \Pr[X \le x \mid Y=y]$$

Note that F'(x|Y=y) is different from the conditional cdf F(x|Y=y), previously defined, but there is a slight problem. The event, Y=y, has zero probability for continuous random variables, hence probability conditional on Y=y is not directly defined and F'(x|Y=y) cannot be found by direct application of event-based probability. However all is OK if we consider it as a limiting case:

$$egin{array}{lll} F'(x|Y=y) &=& \displaystyle \liminf_{\delta(y) o 0} \, \Pr[X\leq x\mid y< Y\leq y+\delta(y)] \ &=& \displaystyle \liminf_{\delta(y) o 0} rac{F(x,y+\delta(y))-F(x,y)}{F_Y(y+\delta(y))-F_Y(y)} \ &=& \displaystyle rac{rac{\partial F(x,y)}{\partial y}}{f_Y(y)} \end{array}$$

Joint and conditional pdfs have similar properties and interpretation to ordinary pdfs:

$$f(x,y)>0$$
 
$$\int\int f(x,y) \mathrm{d} x \mathrm{d} y = 1$$
 
$$f(x|y)>0$$
 
$$\int f(x|y) \mathrm{d} x = 1$$

**Note:**From now on interpret  $\int$  as  $\int_{-\infty}^{\infty}$  unless otherwise stated.

For pdfs we get the following rules:

• Conditional pdf: Equation:

$$f(x|y) = \frac{f(x,y)}{f(y)}$$

• Bayes Rule (pdf): Equation:

$$f(x|y) = \frac{f(y|x)f(x)}{f(y)}$$

• Total Probability (pdf): Equation:

$$\int f(y|x)f(x) dx = \int f(y,x) dx$$
$$= f(y) \int f(x|y) dx$$
$$= f(y)$$

The final result is often referred to as the Marginalisation Integral and f(y) as the Marginal Probability.

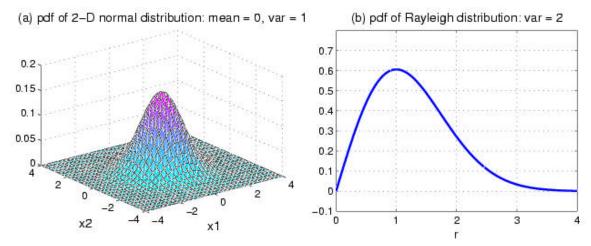
#### Random Vectors

Random Vectors are simply groups of random variables, arranged as vectors. E.g.: **Equation:** 

$$oldsymbol{X} = (X_1 \quad \dots \quad X_n)^T$$

where  $X_1, \ldots X_n$  are n separate random variables.

In general, all of the previous results can be applied to random vectors as well as to random scalars, but vectors allow some interesting new results too.



pdfs of (a) a 2-D normal distribution and (b) a Rayleigh distribution, corresponding to the magnitude of the 2-D random vectors.

# **Example - Arrows on a target**

Suppose that arrows are shot at a target and land at random distances from the target centre. The horizontal and vertical components of these distances are formed into a 2-D random error vector. If each component of this error vector is an independent variable with zero-mean Gaussian pdf of variance  $\sigma^2$ , calculate the pdf's of the radial magnitude and the phase angle of the error vector.

Let the error vector be

$$oldsymbol{X} = egin{pmatrix} X_1 & X_2 \end{pmatrix}^T$$

 $X_1$  and  $X_2$  each have a zero-mean Gaussian pdf given by **Equation:** 

$$f(x)=rac{1}{\sqrt{2\pi\sigma^2}}e^{-rac{x^2}{2\sigma^2}}$$

Since  $X_1$  and  $X_2$  are independent, the 2-D pdf of  $\boldsymbol{X}$  is **Equation:** 

$$egin{array}{lll} f_X(x_1,x_2) &=& f(x_1)f(x_2) \ &=& rac{1}{2\pi\sigma^2}e^{-rac{x_1^2+x_2^2}{2\sigma^2}} \end{array}$$

In polar coordinates

$$x_1 = r\cos(\theta)$$

and

$$x_2 = r\sin( heta)$$

To calculate the radial pdf, we substitute  $r=\sqrt{{x_1}^2+{x_2}^2}$  in the above 2-D pdf to get:

### **Equation:**

$$\Pr[r < R < r + \delta(r)] = \int_r^{r + \delta(r)} \int_{-\pi}^{\pi} f_X(x_1, x_2) R \; \mathrm{d} \; heta \; \mathrm{d} \; R$$

where

$$\int_{r}^{r+\delta(r)} \int_{-\pi}^{\pi} f_X(x_1,x_2) R \; \mathrm{d} \; \theta \; \mathrm{d} \; R \simeq \delta(r) \int_{-\pi}^{\pi} \frac{1}{2\pi\sigma^2} e^{-\frac{r^2}{2\sigma^2}} r \; \mathrm{d} \; \theta = \frac{1}{\sigma^2} r e^{-\frac{r^2}{2\sigma^2}} \delta(r)$$

Hence the radial pdf of the error vector is:

$$egin{array}{lll} f_R(r) &=& rac{\lim _{\delta(r) 
ightarrow 0} \Pr[r < R < r + \delta(r)]}{\delta(r)} \ &=& rac{1}{\sigma^2} r e^{-rac{r^2}{2\sigma^2}} \end{array}$$

This is a **Rayleigh distribution** with variance =  $2\sigma^2$  (these are two components of  $\boldsymbol{X}$ , each with variance  $\sigma^2$ ).

The 2-D pdf of X depends only on r and not on  $\theta$ , so the angular pdf of the error vector is constant over any  $2\pi$  interval and is therefore

$$f_{\Theta}( heta) = rac{1}{2\pi}$$

so that

$$\int_{-\pi}^{\pi} f_{\Theta}(\theta) \; \mathrm{d} \; \theta = 1$$

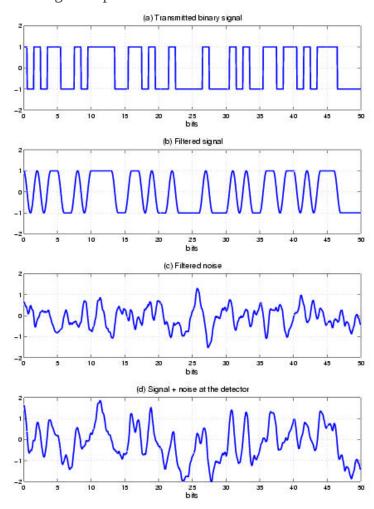
#### Random Signals

Random signals are random variables which evolve, often with time (e.g. audio noise), but also with distance (e.g. intensity in an image of a random texture), or sometimes another parameter.

They can be described as usual by their cdf and either their pmf (if the amplitude is discrete, as in a digitized signal) or their pdf (if the amplitude is continuous, as in most analogue signals).

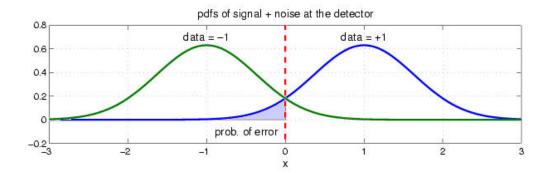
However a very important additional property is how rapidly a random signal fluctuates. Clearly a slowly varying signal such as the waves in an ocean is very different from a rapidly varying signal such as vibrations in a vehicle. We will see later in [link] how to deal with these frequency dependent characteristics of randomness.

For the moment we shall assume that random signals are sampled at regular intervals and that each signal is equivalent to a sequence of samples of a given random process, as in the following examples.



Detection of cianals in noise. (a) the transmitted

binary signal; (b) the binary signal after filtering with a half-sine receiver filter; (c) the channel noise after filtering with the same filter; (d) the filtered signal plus noise at the detector in the receiver.



The pdfs of the signal plus noise at the detector for the two  $\pm(1)$ . The vertical dashed line is the detector threshold and the shaded area to the left of the origin represents the probability of error when data = 1.

### **Example - Detection of a binary signal in noise**

We now consider the example of detecting a binary signal after it has passed through a channel which adds noise. The transmitted signal is typically as shown in (a) of [link].

In order to reduce the channel noise, the receiver will include a lowpass filter. The aim of the filter is to reduce the noise as much as possible without reducing the peak values of the signal significantly. A good filter for this has a half-sine impulse response of the form:

#### **Equation:**

$$h(t) = egin{cases} rac{\pi}{2T_b} \sin\!\left(rac{\pi t}{T_b}
ight) & ext{if} \;\; 0 \leq t \leq T_b \ 0 & ext{otherwise} \end{cases}$$

Where  $T_b$  = bit period.

This filter will convert the rectangular data bits into sinusoidally shaped pulses as shown in (b) of [link] and it will also convert wide bandwidth channel noise into the form shown in (c) of [link]. Bandlimited noise of this form will usually have an approximately Gaussian pdf.

Because this filter has an impulse response limited to just one bit period and has unit gain at zero frequency (the area under h(t) is unity), the signal values at the center of each bit period at the detector will still be  $\pm(1)$ . If we choose to sample each bit at the detector at this optimal mid point, the pdfs of the signal plus noise at the detector will be shown in  $[\underline{link}]$ .

Let the filtered data signal be D(t) and the filtered noise be U(t), then the detector signal is **Equation:** 

$$R(t) = D(t) + U(t)$$

If we assume that +(1) and -1 bits are equiprobable and the noise is a symmetric zeromean process, the optimum detector threshold is clearly midway between these two states, i.e. at zero. The probability of error when the data = +(1) is then given by:

#### **Equation:**

$$egin{array}{lll} \Pr[\mathrm{error} \ | \ D = + (1)] &= & \Pr[R(t) < 0 \ | \ D = + (1)] \ &= & F_U(-1) \ &= & \int_{-\infty}^{-1} f_U(u) \ \mathrm{d} \ u \end{array}$$

where  $F_U$  and  $f_U$  are the cdf and pdf of U. This is the shaded area in [link].

Similarly the probability of error when the data = -1 is then given by:

#### **Equation:**

$$egin{array}{lll} \Pr[\mathrm{error} \mid D = -1] &=& \Pr[R(t) > 0 \mid D = -1] \ &=& 1 - F_U(+(1)) \ &=& \int_1^\infty f_U(u) \; \mathrm{d} \; u \end{array}$$

Hence the overall probability of error is:

#### **Equation:**

$$\begin{array}{lll} \Pr[\text{error}] & = & \Pr[\text{error} \mid D = +(1)] \Pr[D = +(1)] + \Pr[\text{error} \mid D = -1] \Pr[D = -1] \\ & = & \int_{-\infty}^{-1} f_U(u) \; \mathrm{d} \; u \Pr[D = +(1)] + \int_{1}^{\infty} f_U(u) \; \mathrm{d} \; u \Pr[D = -1] \end{array}$$

since  $f_U$  is symmetric about zero

$$\Pr[ ext{error}] = \int_1^\infty f_U(u) \; \mathrm{d} \; u \left( \Pr[D = +(1)] + \Pr[D = -1] 
ight) = \int_1^\infty f_U(u) \; \mathrm{d} \; u$$

To be a little more general and to account for signal attenuation over the channel, we shall assume that the signal values at the detector are  $\pm(v_0)$  (rather than  $\pm(1)$ ) and that the filtered noise at the detector has a zero-mean Gaussian pdf with variance  $\sigma^2$ :

#### **Equation:**

$$f_U(u) = rac{1}{\sqrt{2\pi\sigma^2}}e^{-rac{u^2}{2\sigma^2}}$$

and so

### **Equation:**

$$egin{array}{lll} ext{Pr[error]} &=& \int_{v_0}^{\infty} f_U(u) \; \mathrm{d} \; u \ &=& \int_{rac{v_0}{\sigma}}^{\infty} f_U(\sigma u) \sigma \; \mathrm{d} \; u \ &=& Qig(rac{v_0}{\sigma}ig) \end{array}$$

where

#### **Equation:**

$$Q(x)=rac{1}{\sqrt{2\pi}}\int_x^\infty e^{-rac{u^2}{2}}\;\mathrm{d}\;u$$

This integral has no analytic solution, but a good approximation to it exists and is discussed in some detail in [link].

From [link] we may obtain the probability of error in the binary detector, which is often expressed as the **bit error rate** or **BER**. For example, if  $\Pr[\text{error}] = 2 \times 10^3$ , this would often be expressed as a bit error rate of  $2 \times 10^3$ , or alternatively as 1 error in 500 bits (on average).

The argument  $(\frac{v_0}{\sigma})$  in  $[\underline{link}]$  is the signal-to-noise voltage ratio (SNR) at the detector, and the BER rapidly diminishes with increasing SNR (see  $[\underline{link}]$ ).

# Approximation Formula for the Gaussian Error Integral, Q(x)

A Gaussian pdf with unit variance is given by:

### **Equation:**

$$f(x)=rac{1}{\sqrt{2\pi}}e^{-rac{x^2}{2}}$$

The probability that a signal with a pdf given by f(x) lies above a given threshold x is given by the Gaussian Error Integral or Q function:

# **Equation:**

$$Q(x) = \int_{x}^{\infty} f(u) \mathrm{~d} \ u$$

There is no analytical solution to this integral, but it has a simple relationship to the error function,  $\operatorname{erf}(x)$ , or its complement,  $\operatorname{erfc}(x)$ , which are tabulated in many books of mathematical tables.

# **Equation:**

$$\operatorname{erf}\left(x
ight) = rac{2}{\sqrt{\pi}} \int_{0}^{x} e^{-u^{2}} \; \mathrm{d} \; u$$

and

# **Equation:**

$$\operatorname{erfc}\left(x
ight) \;\;=\;\; 1-\operatorname{erf}\left(x
ight) \ =\;\; rac{2}{\sqrt{\pi}}\int_{x}^{\infty}e^{-u^{2}}\;\mathrm{d}\;u$$

Therefore,

$$egin{array}{lll} Q(x) &=& rac{1}{2}\operatorname{erfc}\left(rac{x}{\sqrt{2}}
ight) \ &=& rac{1}{2}\left(1-\operatorname{erf}\left(rac{x}{\sqrt{2}}
ight)
ight) \end{array}$$

Note that  $\operatorname{erf}(0) = 0$  and  $\operatorname{erf}(\infty) = 1$ , and therefore Q(0) = 0.5 and  $Q(x) \to 0$  very rapidly as x becomes large.

It is useful to derive simple approximations to Q(x) which can be used on a calculator and avoid the need for tables.

Let v = u - x, then:

### **Equation:**

$$egin{array}{lll} Q(x) & = & \int_0^\infty f(v+x) \; \mathrm{d} \; v \ & = & rac{1}{\sqrt{2\pi}} \int_0^\infty e^{-rac{v^2+2vx+x^2}{2}} \; \mathrm{d} \; v \ & = & rac{e^{-rac{x^2}{2}}}{\sqrt{2\pi}} \int_0^\infty e^{-(vx)} e^{-rac{v^2}{2}} \; \mathrm{d} \; v \end{array}$$

Now if  $x\gg 1$ , we may obtain an approximate solution by replacing the  $e^{-\frac{v^2}{2}}$  term in the integral by unity, since it will initially decay much slower than the  $e^{-(vx)}$  term. Therefore

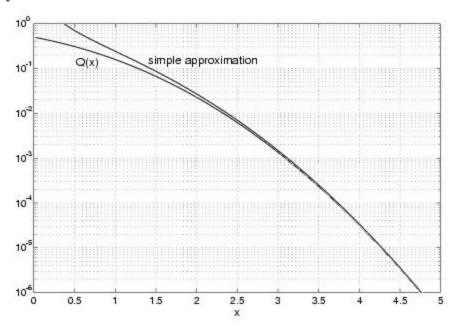
# **Equation:**

$$Q(x) < rac{e^{-rac{x^2}{2}}}{\sqrt{2\pi}} \int_0^\infty e^{-(vx)} \; \mathrm{d} \; v = rac{e^{-rac{x^2}{2}}}{\sqrt{2\pi}x}$$

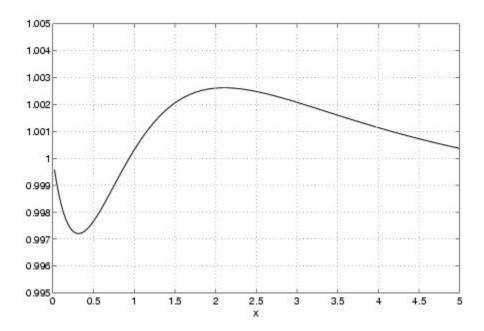
This approximation is an upper bound, and its ratio to the true value of Q(x) becomes less than 1.1 only when x>3, as shown in [link]. We may obtain a much better approximation to Q(x) by altering the denominator above from ( $\sqrt{2\pi}x$ ) to ( $1.64x + \sqrt{0.76x^2 + 4}$ ) to give:

$$Q(x) \simeq rac{e^{-rac{x^2}{2}}}{1.64x + \sqrt{0.76x^2 + 4}}$$

This improved approximation gives a curve indistinguishable from Q(x) in  $[\underline{\operatorname{link}}]$  and its ratio to the true Q(x) is now within  $\pm (0.3\%)$  of unity for all  $x \geq 0$  as shown in  $[\underline{\operatorname{link}}]$ . This accuracy is sufficient for nearly all practical problems.



Q(x) and the simple approximation of [link].



The ration of the improved approximation of Q(x) in  $[\underline{\text{link}}]$  to the true value, obtained by numerical integration.

# Expectation

Expectations form a fundamental part of random signal theory. In simple terms the **Expectation Operator** calculates the **mean** of a random quantity although the concept turns out to be much more general and useful than just this.

If X has pdf  $f_X(x)$  (correctly normalised so that  $\int_{-\infty}^{\infty} f_X(x) dx = 1$ ), its expectation is given by:

### **Equation:**

$$egin{array}{lll} E[X] &=& \int_{-\infty}^{\infty} x f_X(x) \; \mathrm{d} \; x \ &=& X \end{array}$$

For discrete processes, we substitute <u>this previous equation</u> in here to get **Equation**:

$$egin{array}{lll} E[X] &=& \int_{-\infty}^{\infty} x \sum_{i=1}^{M} p_X(x_i) \delta(x-x_i) \; \mathrm{d} \; x \ &=& \sum_{i=1}^{M} x_i p_X(x_i) \ &=& X \end{array}$$

Now, what is the mean value of some function, Y = g(X)?

Using the result of <u>this previous equation</u> for pdfs of related processes Y and X:

# **Equation:**

$$f_Y(y) \mathcal{O}(y) = f_X(x) \mathcal{O}(x)$$

Hence (again assuming infinite integral limits unless stated otherwise) **Equation:** 

$$E[g(X)] = E[Y]$$

$$= \int y f_Y(y) d y$$

$$= \int g(x) f_X(x) d x$$

This is an important result which allows us to use the Expectation Operator for many purposes including the calculation of moments and other related parameters of a random process.

Note, expectation is a **Linear Operator**:

$$E[ag_1(X) + bg_2(X)] = aE[g_1(X)] + bE[g_2(X)]$$

# Important Examples of Expectation

We get **Moments** of a pdf by setting  $g(X) = X^n$  in <u>this previous equation</u>, **Equation**:

# nth order moment

$$E[X^n] = \int \, x^n f_X(x) \; \mathrm{d} \; x$$

- n=1: 1st order moment, E[x] = Mean value
- n=2: 2nd order moment,  $E[x^2]$  = Mean-squared value (Power or energy)
- n>2: Higher order moments,  $E[x^n]$ , give more detail about  $f_X(x)$ .

### **Central Moments**

Central moments are moments about the **centre** or mean of a distribution, **Equation:** 

#### nth order central moment

$$Eigg[ig(X-\overline{X}ig)^nigg]=\int ig(x-\overline{X}ig)^n f_X(x) \; \mathrm{d} \; x$$

Some important parameters from central moments of a pdf are:

• Variance, n = 2: **Equation:** 

$$\sigma^{2} = E\left[\left(X - \overline{X}\right)^{2}\right]$$

$$= \int \left(x - \overline{X}\right)^{2} f_{X}(x) d x$$

$$= \int x^{2} f_{X}(x) d x - 2\overline{X} \int x f_{X}(x) d x + \left(\overline{X}\right)^{2} \int f_{X}(x) d x$$

$$= E\left[X^{2}\right] - 2\left(\overline{X}\right)^{2} + \left(\overline{X}\right)^{2}$$

$$= E\left[X^{2}\right] - \left(\overline{X}\right)^{2}$$

- Standard deviation,  $\sigma = \sqrt{\text{variance}}$ .
- Skewness, n=3:

### **Equation:**

$$\gamma = \frac{E\left[\left(X - \overline{X}\right)^3\right]}{\sigma^3}$$

 $\gamma=0$  if the pdf of X is symmetric about  $\overline{X}$ , and becomes more positive if the tail of the distribution is heavier when  $X>\overline{X}$ .

• Kurtosis (or excess), n = 4:

# **Equation:**

$$\kappa = rac{Eigg[ig(X-ar{X}ig)^4igg]}{\sigma^4} - 3$$

 $\kappa=0$  for a Gaussian pdf and becomes more positive for distributions with heavier tails.

**Note:** Skewness and kurtosis are normalized by dividing the central moments by appropriate powers of  $\sigma$  to make them dimensionless. Kurtosis is usually offset by -3 to make it zero for Gaussian pdfs.

# **Example: Central Moments of a Normal Distribution**

The normal (or Gaussian) pdf with zero mean is given by: **Equation:** 

$$f_X(x)=rac{1}{\sqrt{2\pi\sigma^2}}e^{-rac{x^2}{2\sigma^2}}$$

What is the *n*th order central moment for the Gaussian?

Since the mean is zero, the nth order central moment is given by **Equation:** 

$$egin{array}{lll} E[X^n] & = & \int x^n f_X(x) \; \mathrm{d} \; x \ & = & rac{1}{\sqrt{2\pi\sigma^2}} \int x^n e^{-rac{x^2}{2\sigma^2}} \; \mathrm{d} \; x \end{array}$$

 $f_X(x)$  is a function of  $x^2$  and therefore is symmetric about zero. So all the odd-order moments will integrate to zero (including the lst-order moment, giving zero mean). The even-order moments are then given by:

# **Equation:**

$$E[X^n] = rac{2}{\sqrt{2\pi\sigma^2}} \int_0^\infty x^n e^{-rac{x^2}{2\sigma^2}} \mathrm{\,d}\, x$$

where n is even. The integral is calculated by substituting  $u=\frac{x^2}{2\sigma^2}$  to give: **Equation:** 

$$\int_0^\infty x^n e^{-rac{x^2}{2\sigma^2}} \,\mathrm{d}\,x = rac{1}{2} ig(2\sigma^2ig)^{rac{n+1}{2}} \int_0^\infty u^{rac{n-1}{2}} e^{-u} \,\mathrm{d}\,u \ = rac{1}{2} ig(2\sigma^2ig)^{rac{n+1}{2}} ig\Gammaig(rac{n+1}{2}ig)$$

Here  $\Gamma(z)$  is the Gamma function, which is defined as an integral for all real z>0 and is rather like the factorial function but generalized to allow non-integer arguments. Values of the Gamma function can be found in mathematical tables. It is defined as follows:

### **Equation:**

$$\Gamma(z) = \int_0^\infty u^{z-1} e^{-u} \mathrm{d} u$$

and has the important (factorial-like) property that

# **Equation:**

$$\forall z, z \neq 0 : (\Gamma(z+1) = z\Gamma(z))$$

# **Equation:**

$$orall z,z\in \mathbb{Z} \ \wedge \ (z>0): (arGamma(z+1)=z!)$$

The following results hold for the Gamma function (see below for a way to evaluate  $\Gamma(\frac{1}{2})$  etc.):

# **Equation:**

$$\Gamma\!\left(rac{1}{2}
ight) = \sqrt{\pi}$$

# **Equation:**

$$\Gamma(1)=1$$

and hence

**Equation:** 

$$\Gamma\!\left(rac{3}{2}
ight) = rac{\sqrt{\pi}}{2}$$

**Equation:** 

$$\Gamma(2)=1$$

Hence

**Equation:** 

$$E[X^n] = egin{cases} 0 & ext{if} & n = ext{odd} \ rac{1}{\sqrt{\pi}} \left(2\sigma^2
ight)^{rac{n}{2}} arGamma\left(rac{n+1}{2}
ight) & ext{if} & n = ext{even} \end{cases}$$

• Valid pdf, n = 0: **Equation:** 

$$E[X^0] = \frac{1}{\sqrt{\pi}} \Gamma(\frac{1}{2})$$
$$= 1$$

as required for a valid pdf.

**Note:** The normalization factor  $\frac{1}{\sqrt{2\pi\sigma^2}}$  in the expression for the pdf of a unit variance Gaussian (e.g. [link]) arises directly from the above result.

• Mean, *n* = 1: **Equation:** 

$$E[X] = 0$$

so the mean is zero.

• Variance, n=2:

## **Equation:**

$$E\left[\left(X - \overline{X}\right)^{2}\right] = E\left[X^{2}\right]$$

$$= \frac{1}{\sqrt{\pi}} \left(2\sigma^{2}\right) \Gamma\left(\frac{3}{2}\right)$$

$$= \frac{1}{\sqrt{\pi}} \left(2\sigma^{2}\right) \frac{\sqrt{\pi}}{2}$$

$$= \sigma^{2}$$

Therefore standard deviation =  $\sqrt{\text{variance}} = \sigma$ .

• Skewness, n=3:

## **Equation:**

$$E[X^3] = 0$$

so the skewness is zero.

• Kurtosis, n = 4:

## **Equation:**

$$E\left[\left(X - \overline{X}\right)^{4}\right] = E\left[X^{4}\right]$$

$$= \frac{1}{\sqrt{\pi}} \left(2\sigma^{2}\right)^{2} \Gamma\left(\frac{5}{2}\right)$$

$$= \frac{1}{\sqrt{\pi}} \left(2\sigma^{2}\right)^{2} \frac{3\sqrt{\pi}}{4}$$

$$= 3\sigma^{4}$$

Hence

$$\kappa = \frac{E\left[\left(X - \overline{X}\right)^4\right]}{\sigma^4} - 3$$

$$= 3 - 3$$

$$= 0$$

## **Evaluation of the Gamma Function**

From the definition of  $\Gamma$  and substituting  $u=x^2$ :

## **Equation:**

$$egin{array}{lll} arGamma\left(rac{1}{2}
ight) &=& \int_{0}^{\infty}u^{-rac{1}{2}}e^{-u} \; \mathrm{d} \; u \ &=& \int_{0}^{\infty}x^{-1}e^{-x^{2}}2x \; \mathrm{d} \; x \ &=& 2\int_{0}^{\infty}e^{-x^{2}} \; \mathrm{d} \; x \ &=& \int_{-\infty}^{\infty}e^{-x^{2}} \; \mathrm{d} \; x \end{array}$$

Using the following squaring trick to convert this to a 2-D integral in polar coordinates:

## **Equation:**

$$\Gamma^{2}\left(\frac{1}{2}\right) = \int_{-\infty}^{\infty} e^{-x^{2}} dx \int_{-\infty}^{\infty} e^{-y^{2}} dy$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} e^{-(x^{2}+y^{2})} dx dy$$

$$= \int_{-\pi}^{\pi} \int_{0}^{\infty} e^{-r^{2}} r dr d\theta$$

$$= 2\pi \left(-\frac{1}{2}\right) e^{-r^{2}} \Big|_{0}^{\infty}$$

$$= \pi$$

and so (ignoring the negative square root):

$$arGammaigg(rac{1}{2}igg)=\sqrt{\pi}\simeq 1.7725$$

Hence, using  $\Gamma(z+1)=z\Gamma(z)$ :

# **Equation:**

$$\Gamma\left(\left\{\frac{3}{2}, \frac{5}{2}, \frac{7}{2}, \frac{9}{2}, \ldots\right\}\right) = \left\{\frac{1}{2}\sqrt{\pi}, \frac{3}{4}\sqrt{\pi}, \frac{15}{8}\sqrt{\pi}, \frac{105}{16}\sqrt{\pi}, \ldots\right\}$$

The case for z = 1 is straightforward:

## **Equation:**

$$\Gamma(1) = \int_0^\infty u^0 e^{-u} du$$

$$= -e^{-u}|_0^\infty$$

$$= 1$$

SO

$$\Gamma(\{2,3,4,5,\ldots\}) = \{1,2,6,24,\ldots\}$$

#### Sums of Random Variables

Consider the random variable Y formed as the sum of two independent random variables  $X_1$  and  $X_2$ :

### **Equation:**

$$Y = X_1 + X_2$$

where  $X_1$  has pdf  $f_1(x_1)$  and  $X_2$  has pdf  $f_2(x_2)$ .

We can write the joint pdf for y and  $x_1$  by rewriting the conditional probability formula:

## **Equation:**

$$f(y,x_1) = f(y|x_1)f_1(x_1)$$

It is clear that the event 'Y takes the value y conditional upon  $X_1 = x_1$ ' is equivalent to  $X_2$  taking a value  $y - x_1$  (since  $X_2 = Y - X_1$ ). Hence **Equation:** 

$$f(y|x_1) = f_2(y - x_1)$$

Now f(y) may be obtained using the **Marginal Probability** formula (<u>this equation</u> from this discussion of <u>probability density functions</u>). Hence **Equation**:

$$f(y) = f(y|x_1)f_1(x_1) d x_1$$
  
=  $f_2(y-x_1)f_1(x_1) d x_1$   
=  $f_2^*f_1$ 

This result may be extended to sums of three or more random variables by repeated application of the above arguments for each new variable in turn. Since convolution is a commutative operation, for n independent variables we get:

# **Equation:**

$$f(y) = f_n * (f_{n-1} * ... * f_2 * f_1)$$
  
=  $f_n * f_{n-1} * ... * f_2 * f_1$ 

An example of this effect occurs when multiple dice are thrown and the scores are added together. In the 2-dice example of the subfigures a,b,c of this figure in the discussion of probability distributions, we saw how the pmf approximated a triangular shape. This is just the convolution of two uniform 6-point pmfs for each of the two dice.

Similarly if two variables with Gaussian pdfs are added together, we shall show in <u>the discussion</u> of the summation of two or more Gaussian random variables that this produces another Gaussian pdf whose variance is the sum of the two input variances.

#### Characteristic Functions

You have already encountered the **Moment Generating Function** of a pdf in the Part IB probability course. This function was closely related to the **Laplace Transform** of the pdf.

Now we introduce the **Characteristic Function** for a random variable, which is closely related to the **Fourier Transform** of the pdf.

In the same way that Fourier Transforms allow easy manipulation of signals when they are convolved with linear system impulse responses, Characteristic Functions allow easy manipulation of convolved pdfs when they represent sums of random processes.

The **Characteristic Function** of a pdf is defined as: **Equation:** 

$$egin{array}{lll} arPhi_X(u) &=& Eig[e^{iux}ig] \ &=& \int_{-\infty}^{\infty} e^{iux} f_X(x) \; \mathrm{d} \; x \ &=& \mathscr{F}(-u) \end{array}$$

where  $\mathscr{F}(u)$  is the Fourier Transform of the pdf.

Note that whenever  $f_X$  is a valid pdf,  $\Phi(0) = \int f_X(x) dx = 1$ 

Properties of Fourier Transforms apply with -u substituted for  $\omega$ . In particular:

• **Convolution** - (sums of independent rv's) **Equation:** 

$$\left(Y=\sum_{i=1}^N X_i
ight)\Rightarrow (f_Y={f_{X_1}}^*f_{X_2}^*\ldots^*f_{X_N})\Rightarrow \left(arPhi_Y(u)=\prod_{i=1}^N arPhi_{X_i}(u)
ight)$$

• Inversion Equation:

$$f_X(x) = rac{1}{2\pi} \int e^{-(iux)} arPhi_X(u) \; \mathrm{d} \; u$$

Moments Equation:

$$\left(rac{\mathrm{d}^n}{\mathrm{d}\ u^n} arPhi_X(u) = \int\ (ix)^n e^{iux} f_X(x)\ \mathrm{d}\ x
ight) \Rightarrow \left(E[X^n] = \int\ x^n f_X(x)\ \mathrm{d}\ x = rac{1}{i^n} rac{\mathrm{d}^n}{\mathrm{d}\ u^n} arPhi_X(u)igg|_{u=0}
ight)$$

• Scaling If Y = aX,  $f_Y(y) = \frac{f_X(x)}{a}$  from this equation in our previous discussion of functions of random variables, then **Equation:** 

$$\Phi_Y(u) = \int e^{iuy} f_Y(y) dy$$

$$= \int e^{iuax} f_X(x) dx$$

$$= \Phi_X(au)$$

#### Characteristic Function of a Gaussian pdf

The Gaussian or normal distribution is very important, largely because of the **Central Limit Theorem** which we shall prove below. Because of this (and as part of the proof of this theorem) we shall show here that a Gaussian pdf has a Gaussian characteristic function too.

A Gaussian distribution with mean  $\mu$  and variance  $\sigma^2$  has pdf:

#### **Equation:**

$$f(x)=rac{1}{\sqrt{2\pi\sigma^2}}e^{-rac{(x-\mu)^2}{2\sigma^2}}$$

Its characteristic function is obtained as follows, using a trick known as completing the square of the exponent: **Equation:** 

$$egin{array}{lll} arPsi_X(u) & = & Eig[e^{iux}ig] \ & = & \int e^{iux}f_X(x) \ \mathrm{d} \ x \ & = & rac{1}{\sqrt{2\pi\sigma^2}} \int e^{-rac{x^2-2\mu x+\mu^2-2\sigma^2iux}{2\sigma^2}} \ \mathrm{d} \ x \ & = & \left(rac{1}{\sqrt{2\pi\sigma^2}} \int e^{-rac{\left(x-\mu+iu\sigma^2
ight)^2}{2\sigma^2}} \ \mathrm{d} \ x
ight) e^{rac{2iu\sigma^2\mu-u^2\sigma^4}{2\sigma^2}} \ & = & e^{iu\mu}e^{-rac{u^2\sigma^2}{2}} \end{array}$$

since the integral in brackets is similar to a Gaussian pdf and integrates to unity.

Thus the characteristic function of a Gaussian pdf is also Gaussian in magnitude,  $e^{-\frac{u^2\sigma^2}{2}}$ , with standard deviation  $\frac{1}{\sigma}$ , and with a linear phase rotation term,  $e^{iu\mu}$ , whose rate of rotation equals the mean  $\mu$  of the pdf. This coincides with standard results from Fourier analysis of Gaussian waveforms and their spectra (e.g. Fourier transform of a Gaussian waveform with time shift).

#### Summation of two or more Gaussian random variables

If two variables,  $X_1$  and  $X_2$ , with Gaussian pdfs are summed to produce X, their characteristic functions will be multiplied together (equivalent to convolving their pdfs) to give

#### **Equation:**

$$egin{array}{lcl} arPhi_X(u) & = & arPhi_{X_1}(u)arPhi_{X_2}(u) \ & = & e^{iu(\mu_1+\mu_2)}e^{-rac{u^2\left(\sigma_1^2+\sigma_2^2
ight)}{2}} \end{array}$$

This is the characteristic function of a Gaussian pdf with mean (  $\mu_1 + \mu_2$ ) and variance (  $\sigma_1^2 + \sigma_2^2$ ).

Further Gaussian variables can be added and the pdf will remain Gaussian with further terms added to the above expressions for the combined mean and variance.

#### **Central Limit Theorem**

The central limit theorem states broadly that if a large number N of independent random variables of arbitrary pdf, but with equal variance  $\sigma^2$  and zero mean, are summed together and scaled by  $\frac{1}{\sqrt{N}}$  to keep the total energy independent of N, then the pdf of the resulting variable will tend to a zero-mean Gaussian with variance  $\sigma^2$  as N tends to infinity.

This result is obvious from the previous result **if the input pdfs are also Gaussian**, but it is the fact that it applies **for arbitrary input pdfs** that is remarkable, and is the reason for the importance of the Gaussian (or normal) pdf. Noise generated in nature is nearly always the result of summing many tiny random processes (e.g. noise from electron energy transitions in a resistor or transistor, or from distant worldwide thunder storms at a radio antenna) and hence tends to a Gaussian pdf.

Although for simplicity, we shall prove the result only for the case when all the summed processes have the **same** variance and pdfs, the central limit result is more general than this and applies in many cases even when the variance and pdfs are not all the same.

#### **Proof:**

Let  $X_i$  (i=1 to N) be the N independent random processes, each will zero mean and variance  $\sigma^2$ , which are combined to give

#### **Equation:**

$$X = rac{1}{\sqrt{N}} \sum_{i=1}^N X_i$$

Then, if the characteristic function of each input process before scaling is  $\Phi(u)$  and we use [link] to include the scaling by  $\frac{1}{\sqrt{N}}$ , the characteristic function of X is

#### **Equation:**

$$egin{array}{lll} arPhi_X(u) &=& \prod_{i=1}^N arPhi_{Xi} \Big(rac{u}{\sqrt{N}}\Big) \ &=& arPhi^N \Big(rac{u}{\sqrt{N}}\Big) \end{array}$$

Taking logs:

#### **Equation:**

$$\log arPhi_X(u) = N \log arPhiigg(rac{u}{\sqrt{N}}igg)$$

Using Taylor's theorem to expand  $\Phi\left(\frac{u}{\sqrt{N}}\right)$  in terms of its derivatives at u=0 (and hence its moments) gives

#### **Equation:**

$$\Phi\left(\frac{u}{\sqrt{N}}\right) = \Phi(0) + \frac{u}{\sqrt{N}} \frac{\mathrm{d}\,\Phi(0)}{\mathrm{d}} + \frac{1}{2} \left(\frac{u}{\sqrt{N}}\right)^2 \frac{\mathrm{d}\,\Phi(0)}{\mathrm{d}} + \frac{1}{6} \left(\frac{u}{\sqrt{N}}\right)^3 \frac{\mathrm{d}\,\Phi(0)}{\mathrm{d}} + \frac{1}{24} \left(\frac{u}{\sqrt{N}}\right)^4 \frac{\mathrm{d}\,\Phi(0)}{\mathrm{d}} + \frac{1}{24} \left(\frac{u$$

From the Moments property of characteristic functions with zero mean:

· valid pdf

$$\Phi(0) = E[X_i^{\ 0}] = 1$$

· zero mean

$$\Phi'(0) = iE[X_i] = 0$$

variance

$$\Phi(0)'' = i^2 E[X_i^2] = -\sigma^2$$

scaled skewness

$$\Phi(0)^{\prime\prime\prime} = i^3 E[X_i{}^3] = -(i\gamma\sigma^3)$$

scaled kurtosis

$$\Phi(0)^4 = i^4 E[X_i^4] = (\kappa + 3)\sigma^4$$

These are all constants, independent of N, and dependent only on the shape of the pdfs  $f_{X_i}$ .

Substituting these moments into [ $\underline{\text{link}}$ ] and [ $\underline{\text{link}}$ ] and using the series expansion,  $\log(1+x)=x+$  (terms of order  $x^2$  or smaller), gives

#### **Equation:**

$$\begin{split} \log \Phi_X(u) &= N \log \Phi\left(\frac{u}{\sqrt{N}}\right) \\ &= N \log\left(1 - \frac{u^2}{2N}\sigma^2 + **\right) \\ &= N\left(-\frac{u^2\sigma^2}{2N} + **\right) \\ &= -\frac{u^2\sigma^2}{2} + \#\# \end{split}$$

where \*\* represents the terms of order  $N^{-\frac{3}{2}}$  or smaller and ## represents the terms of order  $N^{-\frac{1}{2}}$  or smaller. As  $N\to\infty$ ,

$$\log arPhi_X(u) 
ightarrow - rac{u^2 \sigma^2}{2}$$

Therefore, as  $N \to \infty$ 

#### **Equation:**

$$arPhi_X(u) o e^{-rac{u^2\sigma^2}{2}}$$

Note that, if the input pdfs are symmetric, the skewness will be zero and the error terms will decay as  $N^{-1}$  rather than  $N^{-\frac{1}{2}}$ ; and so convergence to a Gaussian characteristic function will be more rapid.

Hence we may now infer from [link], [link] and [link] that the pdf of X as  $N \to \infty$  will be given by **Equation:** 

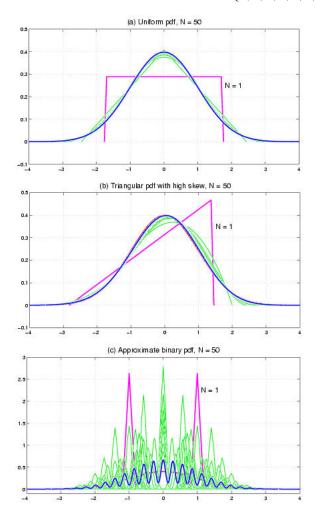
$$f_X(x)=rac{1}{\sqrt{2\pi\sigma^2}}e^{-rac{x^2}{2\sigma^2}}$$

#### Thus we have proved the required central limit result.

[link] shows an example of convergence when the input pdfs are uniform, and N is gradually increased from 1 to 50. By N=12, convergence is good, and this is how some 'Gaussian' random generator functions operate - by summing typically 12 uncorrelated random numbers with uniform pdfs.

For some less smooth or more skewed pdfs, convergence can be slower, as shown for a highly skewed triangular pdf in [link]; and pdfs of discrete processes are particularly problematic in this respect, as illustrated in [link].

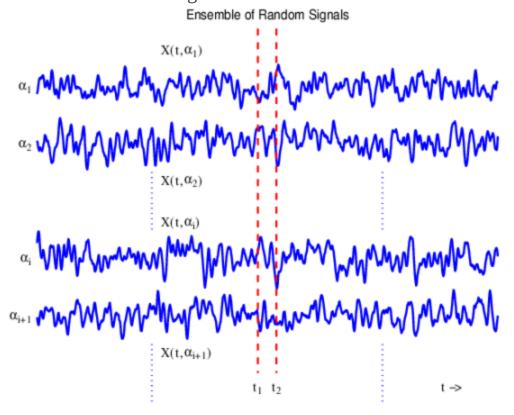
Convergence toward a Gaussian pdf (Central Limit Theorem) for 3 different input pdfs for N=1 to 50. Note that the uniform pdf (a) with smallest higher-order moments converges fastest. Curves are shown for  $N=\{1,2,3,4,6,8,10,12,15,20,30,50\}$ .



#### Random Processes

We discussed Random Signals briefly and now we return to consider them in detail. We shall assume that they evolve continuously with time t, although they may equally well evolve with distance (e.g. a random texture in image processing) or some other parameter.

We can imagine a generalization of our previous ideas about random experiments so that the outcome of an experiment can be a 'Random Object', an example of which is a signal waveform chosen at random from a set of possible signal waveforms, which we term an **Ensemble**. This ensemble of random signals is known as a **Random Process**.



Ensemble representation of a random process.

An example of a Random Process  $X(t, \alpha)$  is shown in [link], where t is time and  $\alpha$  is an index to the various members of the ensemble.

- *t* is assumed to belong to some set (the time axis).
- $\alpha$  is assumed to belong to some set (the sample space).
- If is a continuous set, such as  $\mathbb{R}$  or  $[0, \infty)$ , then the process is termed a **Continuous Time** random process.
- If is a discrete set of time values, such as the integers  $\mathbb{Z}$ , the process is termed a **Discrete Time Process** or **Time Series**.
- The members of the ensemble can be the result of different random events, such as different instances of the sound 'ah' during the course of this lecture. In this case  $\alpha$  is discrete.
- Alternatively the ensemble members are often just different portions of a single random signal. If the signal is a continuous waveform, then  $\alpha$  may also be a continuous variable, indicating the starting point of each ensemble waveform.

We will often drop the explicit dependence on  $\alpha$  for notational convenience, referring simply to **random process**  $\{X(t)\}$ .

If we consider the process  $\{X(t)\}$  at one particular time  $t=t_1$ , then we have a **random variable**  $X(t_1)$ .

If we consider the process  $\{X(t)\}$  at N time instants  $\{t_1, t_2, ..., t_N\}$ , then we have a **random vector**:

$$oldsymbol{X} = egin{pmatrix} X(t_1) & X(t_2) & \dots & X(t_N) \end{pmatrix}^T$$

We can study the properties of a random process by considering the behavior of random variables and random vectors extracted from the process, using the probability theory derived earlier in this course.

#### Correlation and Covariance

Correlation and covariance are techniques for measuring the similarity of one signal to another. For a random process  $X(t, \alpha)$  they are defined as follows.

• Auto-correlation function: Equation:

$$egin{array}{lll} r_{XX}(t_1,t_2) &=& E[X(t_1,lpha)X(t_2,lpha)] \ &=& \int \int x_1x_2f(x_1,x_2) \; \mathrm{d}\; x_1 \; \mathrm{d}\; x_2 \end{array}$$

where the expectation is performed over all  $\alpha \in$  (i.e. the whole ensemble), and  $f(x_1, x_2)$  is the joint pdf when  $x_1$  and  $x_2$  are samples taken at times  $t_1$  and  $t_2$  from the **same random event**  $\alpha$  of the random process X.

• Auto-covariance function: Equation:

$$egin{array}{lll} c_{XX}(t_1,t_2) &=& Eigg[ igg( X(t_1,lpha) - X(t_1) igg) igg( X(t_2,lpha) - X(t_2) igg) igg] \\ &=& \int \int igg( x_1 - X(t_1) igg) igg( x_2 - X(t_2) igg) f(x_1,x_2) \; \mathrm{d} \; x_1 \; \mathrm{d} \; x_2 \\ &=& r_{XX}(t_1,t_2) - 2X(t_1) X(t_2) + X(t_1) X(t_2) \\ &=& r_{XX}(t_1,t_2) - X(t_1) X(t_2) \end{array}$$

where the same conditions apply as for auto-correlation and the means

 $X(t_1)$  and  $X(t_2)$  are taken over all  $\alpha \in .$  Covariances are similar to correlations except that the effects of the means are removed.

• **Cross-correlation function:** If we have two different processes,  $X(t, \alpha)$  and  $Y(t, \alpha)$ , both arising as a result of the same random event  $\alpha$ , then cross-correlation is defined as

$$r_{XY}(t_1, t_2) = E[X(t_1, \alpha)Y(t_2, \alpha)]$$
  
=  $\int \int x_1 y_2 f(x_1, y_2) dx_1 dy_2$ 

where  $f(x_1, y_2)$  is the joint pdf when  $x_1$  and  $y_2$  are samples of X and Y taken at times  $t_1$  and  $t_2$  as a result of the **same random event**  $\alpha$ . Again the expectation is performed over all  $\alpha \in$ .

• Cross-covariance function: Equation:

$$c_{XY}(t_1, t_2) = E\left[\left(X(t_1, \alpha) - X(t_1)\right) \left(Y(t_2, \alpha) - Y(t_2)\right)\right]$$

$$= \int \int \left(x_1 - X(t_1)\right) \left(y_2 - Y(t_2)\right) f(x_1, y_2) d x_1 d y_2$$

$$= r_{XY}(t_1, t_2) - X(t_1)Y(t_2)$$

For Deterministic Random Processes which depend deterministically on the random variable  $\alpha$  (or some function of it), we can simplify the above integrals by expressing the joint pdf in that space. E.g. for auto-correlation:

$$egin{array}{lll} r_{XX}(t_1,t_2) &=& E[X(t_1,lpha)X(t_2,lpha)] \ &=& \int x(t_1,lpha)x(t_2,lpha)f(lpha) \; \mathrm{d} \; lpha \end{array}$$

## Stationarity

Stationarity in a Random Process implies that its statistical characteristics **do not change with time**. Put another way, if one were to observe a stationary random process at some time t it would be impossible to distinguish the **statistical characteristics** at that time from those at some other time t'.

# **Strict Sense Stationarity (SSS)**

Choose a Random Vector of length N from a Random Process:

## **Equation:**

$$oldsymbol{X} = egin{pmatrix} X(t_1) & X(t_2) & \dots & X(t_N) \end{pmatrix}^T$$

Its *N*th order cdf is

### **Equation:**

$$F_{X(t_1),\,\ldots\,X(t_N)}(x_1,\ldots,x_N) = \Pr[\{X(t_1) \le x_1,\ldots,X(t_N) \le x_N\}]$$

X(t) is defined to be **Strict Sense Stationary** iff:

# **Equation:**

$$F_{X(t_1),\,\ldots\,X(t_N)}(x_1,\ldots,x_N) = F_{X(t_1+c),\,\ldots\,X(t_N+c)}(x_1,\ldots,x_N)$$

for all time shifts c, all finite N and all sets of time points  $\{t_1, \ldots, t_N\}$ .

# Wide Sense (Weak) Stationarity (WSS)

If we are only interested in the properties of moments up to 2nd order (mean, autocorrelation, covariance, ...), which is the case for many practical applications, a weaker form of stationarity can be useful:

X(t) is defined to be **Wide Sense Stationary** (or Weakly Stationary) iff:

1. The mean value is independent of t, for all t **Equation:** 

$$E[X(t)] = \mu$$

2. Autocorrelation depends only upon  $au=t_2-t_1$ , for all  $t_1$  **Equation:** 

$$E[X(t_1)X(t_2)] = E[X(t_1)X(t_1+ au)] = r_{XX}( au)$$

Note that, since 2nd-order moments are defined in terms of 2nd-order probability distributions, strict sense stationary processes are **always** widesense stationary, but not necessarily **vice versa**.

## Ergodicity

Many stationary random processes are also **Ergodic**. For an Ergodic Random Process we can exchange **Ensemble Averages** for **Time Averages**. This is equivalent to assuming that our ensemble of random signals is just composed of all possible time shifts of a single signal X(t).

Recall from our previous discussion of <u>Expectation</u> that the expectation of a function of a random variable is given by

### **Equation:**

$$E[g(X)] = \int g(x) f_X(x) \; \mathrm{d} \; x$$

This result also applies if we have a **random function** g(.) of a **deterministic variable** such as t. Hence **Equation:** 

$$E[g(t)] = \int g(t) f_T(t) \; \mathrm{d} \; t$$

Because t is linearly increasing, the pdf  $f_T(t)$  is uniform over our measurement interval, say -T to T, and will be  $\frac{1}{2T}$  to make the pdf valid (integral = 1). Hence

# **Equation:**

$$E[g(t)] = \int_{-T}^{T} g(t) \frac{1}{2T} dt$$
$$= \frac{1}{2T} \int_{-T}^{T} g(t) dt$$

If we wish to measure over all time, then we take the limit as  $T \to \infty$ .

This leads to the following results for Ergodic WSS random processes:

# • Mean Ergodic:

## **Equation:**

$$E[X(t)] = \int_{-\infty}^{\infty} x f_{X(t)}(x) d x$$
$$= \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} X(t) d t$$

• Correlation Ergodic: Equation:

$$egin{array}{lll} r_{XX}( au) &=& E[X(t)X(t+ au)] \ &=& \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x_1 x_2 f_{X(t),X(t+ au)}(x_1,x_2) \; \mathrm{d} \; x_1 \; \mathrm{d} \; x_2 \ &=& \lim_{T 
ightarrow \infty} rac{1}{2T} \int_{-T}^T X(t) X(t+ au) \; \mathrm{d} \; t \end{array}$$

and similarly for other correlation or covariance functions.

**Ergodicity greatly simplifies the measurement of WSS processes** and it is often assumed when estimating moments (or correlations) for such processes.

In almost all practical situations, processes are stationary **only over some limited time interval** (say  $T_1$  to  $T_2$ ) rather than over all time. In that case we deliberately keep the limits of the integral finite and adjust  $f_{X(t)}$  accordingly. For example the autocorrelation function is then measured using

# **Equation:**

$$r_{XX}( au) = rac{1}{T_2 - T_1} \int_{T_1}^{T_2} X(t) X(t + au) \; \mathrm{d} \; t$$

This avoids including samples of X which have incorrect statistics, but it can suffer from errors due to limited sample size.

### Spectral Properties of Random Signals

### **Relation of Power spectral Density to ACF**

The autocorrelation function (ACF) of an ergodic random signal tells us how correlated the signal is with itself as a function of time shift  $\tau$ . In particular, for  $\tau=0$  **Equation:** 

$$egin{array}{lll} r_{XX}(0) &=& \displaystyle \liminf_{T o \infty} \, rac{1}{2T} \int_{-T}^T X^2(t) \, \mathrm{d} \, t \ &=& \mathrm{mean \ power \ of \ } \mathrm{X}(\mathrm{t}) \end{array}$$

Note that if  $T \to \infty$ , for all  $\tau$ 

### **Equation:**

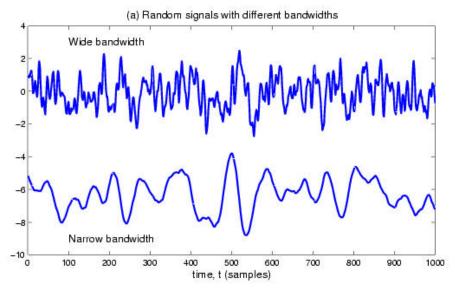
$$r_{XX}( au) = r_{XX}(- au) \le r_{XX}(0)$$

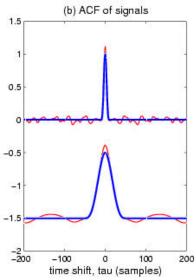
As  $\tau$  becomes large, X(t) and  $X(t+\tau)$  will usually become decorrelated and, as long as X is zero mean,  $r_{XX}$  will tend to zero.

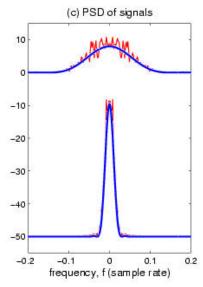
Hence the ACF will have its **maximum at**  $\tau=0$  and decay symmetrically to zero (or to  $\mu^2$ , if  $\mu\neq 0$ ) as  $|\tau|$  increases.

The width of the ACF (to say its half-power points) tells us how slowly X is fluctuating or how band-limited it is. [link] shows how the ACF of a rapidly fluctuating (wideband) random signal, as in [link] upper plot, decays quickly to zero as  $|\tau|$  increases, whereas, for a slowly fluctuating signal, as in [link] lower plot, the ACF decays much more slowly.

Illustration of the different properties of wide band (upper) and narrow band (lower) random signals: (a) the signal waveforms with unit variance; (b) their autocorrelation functions (ACFs); and (c) their power spectral densities (PSDs). In (b) and (c), the thin fluctuating curves shows the actual values measured from 4000 samples of the random waveforms while the thick smooth curves show the limits of the ACF and PSD as the lengths of the waveforms tend to infinity.







The ACF measures an entirely different aspect of randomness from amplitude distributions such as pdf and cdf.

As with deterministic signals, we may formalize our ideas of rates of fluctuation by transforming to the **Frequency (Spectral) Domain** using the **Fourier Transform**: **Equation**:

$$\mathscr{F}_{u}(\omega) = \operatorname{FT}(u(t))$$
  
=  $\int u(t)e^{-(i\omega t)} dt$ 

The **Power Spectral Density** (PSD) of a random process *X* is defined to be the Fourier Transform of its ACF:

#### **Equation:**

$$S_X(\omega) = \operatorname{FT}(r_{XX}(\tau))$$
  
=  $\int r_{XX}(\tau)e^{-(i\omega\tau)} d\tau$ 

**Equation:** 

$$egin{array}{lll} r_{XX}( au) &=& \mathrm{FT^{-1}}(S_X(\omega)) \ &=& rac{1}{2\pi}\int S_X(\omega)e^{i\omega au} \;\mathrm{d}\;\omega \end{array}$$

N.B.  $\{X(t)\}$  must be **at least** Wide Sense Stationary (WSS).

From [link] and [link] we see that the mean signal power is given by: **Equation:** 

$$r_{XX}(0) = \frac{1}{2\pi} \int S_X(\omega) d\omega$$
  
=  $\int S_X(2\pi f) df$ 

Hence  $S_X$  has units of power per Hertz. Note that we must integrate over **all** frequencies, both positive and negative, to get the correct total power.

[link] shows how the PSDs of the signals relate to the ACFs in [link].

Properties of PSDs for real-valued X(t):

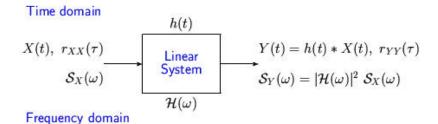
1. 
$$S_X(\omega) = S_X(-\omega)$$

2. 
$$S_X(\omega)$$
 is Real-valued

$$3. S_X(\omega) \geq 0$$

Properties 1 and 2 are because ACFs are real and symmetric about  $\tau = 0$ ; and 3 is because  $S_X$  represents **power** density.

# Linear system (filter) with WSS input



Block diagram of a linear system with a random input signal, X(t).

Let the linear system with input X(t) and output Y(t) have an impulse response h(t), so

### **Equation:**

$$Y(t) = h(t)*X(t)$$
  
=  $\int h(\alpha)X(t-\alpha) d\alpha$ 

Then the ACF of Y is

#### **Equation:**

$$\begin{array}{ll} r_{YY}(t_1,t_2) &=& E[Y(t_1)Y(t_2)] \\ &=& E\left[\int h(\alpha_1)X(t_1-\alpha_1) \ \mathrm{d} \ \alpha_1 \int h(\alpha_2)X(t_2-\alpha_2) \ \mathrm{d} \ \alpha_2\right] \\ &=& E\left[\int \int h(\alpha_1)h(\alpha_2)X(t_1-\alpha_1)X(t_2-\alpha_2) \ \mathrm{d} \ \alpha_1 \ \mathrm{d} \ \alpha_2\right] \\ &=& \int \int h(\alpha_1)h(\alpha_2)E[X(t_1-\alpha_1)X(t_2-\alpha_2)] \ \mathrm{d} \ \alpha_1 \ \mathrm{d} \ \alpha_2 \\ &=& \int \int h(\alpha_1)h(\alpha_2)r_{XX}(t_1-\alpha_1,t_2-\alpha_2) \ \mathrm{d} \ \alpha_1 \ \mathrm{d} \ \alpha_2 \end{array}$$

If *X* is WSS then

$$egin{array}{lll} r_{YY}( au) &=& E[Y(t)Y(t+ au)] \ &=& \int\int h(lpha_1)h(lpha_2)r_{XX}( au+lpha_1-lpha_2) \; \mathrm{d} \; lpha_1 \; \mathrm{d} \; lpha_2 \ &=& r_{XX}( au)^*h(- au)^*h( au) \end{array}$$

Taking Fourier transforms:

#### **Equation:**

$$\begin{split} S_Y(\omega) &= \operatorname{FT}(r_{YY}(\tau)) \\ &= \int \int \int h(\alpha_1)h(\alpha_2)r_{XX}(\tau+\alpha_1-\alpha_2) \operatorname{d}\alpha_1 \operatorname{d}\alpha_2 e^{-(i\omega\tau)} \operatorname{d}\tau \\ &= \int \int h(\alpha_1)h(\alpha_2) \int r_{XX}(\tau+\alpha_1-\alpha_2) e^{-(i\omega\tau)} \operatorname{d}\tau \operatorname{d}\alpha_1 \operatorname{d}\alpha_2 \\ &= \int \int h(\alpha_1)h(\alpha_2) \int r_{XX}(\lambda) e^{-(i\omega(\lambda-\alpha_1+\alpha_2))} \operatorname{d}\lambda \operatorname{d}\alpha_1 \operatorname{d}\alpha_2 \\ &= \int h(\alpha_1)e^{i\omega\alpha_1} \operatorname{d}\alpha_1 \int h(\alpha_2) e^{-(i\omega\alpha_2)} \operatorname{d}\alpha_2 \int r_{XX}(\lambda) e^{-(i\omega\lambda)} \operatorname{d}\lambda \\ &= \overline{\mathscr{H}(\omega)}\mathscr{H}(\omega)S_X(\omega) \end{split}$$

where  $\mathcal{H}(\omega) = \mathrm{FT}\,(h(t))$ . i.e:

#### **Equation:**

$$S_Y(\omega) = (|\mathscr{H}(\omega)|)^2 S_X(\omega)$$

Hence the PSD of Y = the PSD of  $X \times$  the power gain  $(|\mathcal{H}|)^2$  of the system at frequency  $\omega$ .

Thus if a large and important system is subject to random perturbations (e.g. a power plant subject to random load fluctuations), we may measure  $r_{XX}(\tau)$  and  $r_{YY}(\tau)$ , transform these to  $S_X(\omega)$  and  $S_Y(\omega)$ , and hence obtain

#### **Equation:**

$$|\mathscr{H}(\omega)| = \sqrt{rac{S_Y(\omega)}{S_X(\omega)}}$$

Hence we may measure the system frequency response without taking the plant off line. But this does not give any information about the phase of  $\mathcal{H}(\omega)$ .

However, if instead we measure the **Cross-Correlation Function** (CCF) between X and Y, we get:

$$egin{array}{lll} r_{XY}(t_1,t_2) &=& E[X(t_1)Y(t_2)] \ &=& Eig[X(t_1)\int h(lpha_2)X(t_2-lpha_2) \; \mathrm{d} \; lpha_2ig] \ &=& Eig[\int h(lpha_2)X(t_1)X(t_2-lpha_2) \; \mathrm{d} \; lpha_2ig] \ &=& \int h(lpha_2)E[X(t_1)X(t_2-lpha_2)] \; \mathrm{d} \; lpha_2 \ &=& \int h(lpha_2)r_{XX}(t_1,t_2-lpha_2) \; \mathrm{d} \; lpha_2 \end{array}$$

If X(t), and hence Y(t), are WSS:

#### **Equation:**

$$r_{XY}(\tau) = E[X(t)Y(t+\tau)]$$
  
=  $\int h(\alpha)r_{XX}(\tau-\alpha) d\alpha$   
=  $h(\tau)^*r_{XX}(\tau)$ 

and taking Fourier transforms:

#### **Equation:**

$$egin{array}{lll} S_{XY}(\omega) &=& \mathrm{FT}\left(r_{XY}( au)
ight) \ &=& \mathscr{H}(\omega)S_X(\omega) \end{array}$$

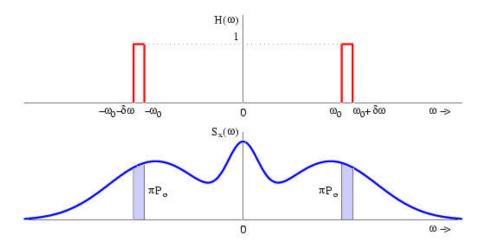
where  $S_{XY}(\omega)$  is known as the **Cross Spectral Density** between X and Y. Therefore, **Equation:** 

$$\mathscr{H}(\omega) = rac{S_{XY}(\omega)}{S_X(\omega)}$$

Hence we obtain the **amplitude and phase** of  $\mathcal{H}(\omega)$ . As before, this is achieved without taking the plant off line.

Note that for WSS processes,  $r_{XY}(\tau) = r_{YX}(-\tau)$  and that (unlike  $r_{XX}$  and  $r_{YY}$ ) these need not be symmetric about  $\tau = 0$ . Hence the cross spectral density  $S_{XY}(\omega)$  need not be purely real (unlike  $S_X(\omega)$ ), and the phase of  $S_{XY}(\omega)$  gives the phase of  $\mathscr{H}(\omega)$ .

# **Physical Interpretation of Power Spectral Density**



Narrowband filter frequency response and PSD of filter input and output.

Let us pass X(t) through a narrow-band filter of bandwidth  $\delta(\omega)=2\pi\delta(f)$ , as shown in [link]:

### **Equation:**

$$\mathscr{H}(\omega) = egin{cases} 1 & ext{if} \;\; \omega_0 < |\omega| \leq \omega_0 + \delta(\omega) \ 0 & ext{otherwise} \end{cases}$$

Find average power at the filter output (shaded area in [link], divided by  $2\pi$ ):

## **Equation:**

$$egin{array}{lll} P_0 &=& r_{YY}(0) \ &=& rac{1}{2\pi} \int_{-\infty}^{\infty} S_Y(\omega) \ \mathrm{d} \ \omega \ &=& rac{1}{2\pi} \int_{-\infty}^{\infty} S_X(\omega) (|\mathscr{H}(\omega)|)^2 \ \mathrm{d} \ \omega \ &=& rac{1}{2\pi} \left( \int_{-(\omega_0+\delta(\omega_0))}^{-\omega_0} S_X(\omega) \ \mathrm{d} \ \omega + \int_{\omega_0}^{\omega_0+\delta(\omega_0)} S_X(\omega) \ \mathrm{d} \ \omega 
ight) \simeq 2 S_X(\omega_0) imes rac{1}{2\pi} \delta(\omega_0) \end{array}$$

since  $S_X(-\omega)=S_X(\omega)$ . Expressed in terms of  $f_0=rac{\omega_0}{2\pi}$ :

$$P_0 \simeq 2 S_X(2\pi f_0) \delta(f)$$

with the factor of 2 appearing because our filter responds to both negative and positive frequency components of X.

Hence  $S_X$  is indeed a **Power Spectral Density** with units  $\frac{V^2}{\mathrm{Hz}}$  (assuming unit impedance).

#### White and Coloured Processes

### White Noise

If we have a zero-mean Wide Sense Stationary process X, it is a **White Noise Process** if its ACF is a delta function at  $\tau = 0$ , i.e. it is of the form: **Equation:** 

$$r_{XX}( au) = P_X \delta( au)$$

where  $P_X$  is a constant.

The PSD of X is then given by

### **Equation:**

$$S_X(\omega) = \int P_X \delta(\tau) e^{-(i\omega\tau)} d\tau$$
  
=  $P_X e^{-(i\omega 0)}$   
=  $P_X$ 

Hence X is **white**, since it contains equal power at **all** frequencies, as in **white light**.

 $P_X$  is the PSD of X at all frequencies.

But:

# **Equation:**

Power of X = 
$$\frac{1}{2\pi} \int_{-\infty}^{\infty} S_X(\omega) d\omega$$
  
=  $\infty$ 

so the White Noise Process is unrealizable in practice, because of its infinite bandwidth.

However, it is very useful as a conceptual entity and as an approximation to 'nearly white' processes which have finite bandwidth, but which are 'white' over all frequencies of practical interest. For 'nearly white' processes,  $r_{XX}(\tau)$  is a narrow pulse of non-zero width, and  $S_X(\omega)$  is flat from zero up to some relatively high cutoff frequency and then decays to zero above that.

### Strict Whiteness and i.i.d. Processes

Usually the above concept of whiteness is sufficient, but a much stronger definition is as follows:

Pick a set of times  $\{t_1, t_2, ..., t_N\}$  to sample X(t).

If, for **any choice** of  $\{t_1, t_2, ..., t_N\}$  with N finite, the random variables  $X(t_1), X(t_2), ..., X(t_N)$  are **jointly independent**, i.e. their joint pdf is given by

### **Equation:**

$$f_{X(t_1),X(t_2),\,\ldots\,X(t_N)}(x_1,x_2,\ldots,x_N) = \prod_{i=1}^N f_{X(t_i)}(x_i)$$

and the marginal pdfs are identical, i.e.

## **Equation:**

$$egin{array}{lcl} f_{X(t_1)} & = & f_{X(t_2)} \ & = & \dots \ & = & f_{X(t_N)} \ & = & f_X \end{array}$$

then the process is termed **Independent and Identically Distributed** (i.i.d).

If, in addition,  $f_X$  is a pdf with zero mean, we have a **Strictly White Noise Process**.

An i.i.d. process is 'white' because the variables  $X(t_i)$  and  $X(t_j)$  are jointly independent, even when separated by an infinitesimally small interval between  $t_i$  and  $t_j$ .

# Additive White Gaussian Noise (AWGN)

In many systems the concept of **Additive White Gaussian Noise (AWGN)** is used. This simply means a process which has a Gaussian pdf, a white PSD, and is linearly added to whatever signal we are analysing.

Note that although 'white' and Gaussian' often go together, this is **not necessary** (especially for 'nearly white' processes).

E.g. a very high speed random bit stream has an ACF which is approximately a delta function, and hence is a nearly white process, but its pdf is clearly not Gaussian - it is a pair of delta functions at +(V) and -V, the two voltage levels of the bit stream.

Conversely a nearly white Gaussian process which has been passed through a lowpass filter (see next section) will still have a Gaussian pdf (as it is a summation of Gaussians) but will no longer be white.

## **Coloured Processes**

A random process whose PSD is not white or nearly white, is often known as a **coloured noise** process.

We may obtain coloured noise Y(t) with PSD  $S_Y(\omega)$  simply by passing white (or nearly white) noise X(t) with PSD  $P_X$  through a filter with frequency response  $\mathscr{H}(\omega)$ , such that from this equation from our discussion of Spectral Properties of Random Signals.

$$S_Y(\omega) = S_X(\omega)(|\mathcal{H}(\omega)|)^2$$
  
=  $P_X(|\mathcal{H}(\omega)|)^2$ 

Hence if we design the filter such that

## **Equation:**

$$|\mathscr{H}(\omega)| = \sqrt{rac{S_Y(\omega)}{P_X}}$$

then Y(t) will have the required coloured PSD.

For this to work,  $S_Y(\omega)$  need only be constant (white) over the passband of the filter, so a **nearly white** process which satisfies this criterion is quite satisfactory and realizable.

Using <u>this equation</u> from our discussion of Spectral Properties of Random Signals and <u>[link]</u>, the ACF of the coloured noise is given by

### **Equation:**

$$r_{YY}(\tau) = r_{XX}(\tau) *h(-\tau) *h(\tau)$$

$$= P_X \delta(\tau) *h(-\tau) *h(\tau)$$

$$= P_X h(-\tau) *h(\tau)$$

where  $h(\tau)$  is the impulse response of the filter.

This Figure from previous discussion shows two examples of coloured noise, although the upper waveform is more 'nearly white' than the lower one, as can be seen in part c of this figure from previous discussion in which the upper PSD is flatter than the lower PSD. In these cases, the coloured waveforms were produced by passing uncorrelated random noise samples (white up to half the sampling frequency) through half-sine filters (as in this equation from our discussion of Random Signals) of length  $T_b = 10$  and 50 samples respectively.